# Weak Formulation of Roe-7 Scheme L'CADAME Weekly Meetings

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Laboratório de Computação de Alto Desempenho e Aprendizado de Máquina em Engenharia (L'CADAME) Weekly Meetings



#### **Governing equation**

• Generic equations for 1-dimensional iso-thermal 2-fluid model

$$\frac{\partial \alpha_g}{\partial t} + u_i \frac{\partial \alpha_g}{\partial x} = 0 \tag{1}$$

$$\frac{\partial \alpha_k \rho_k}{\partial t} + \frac{\partial \alpha_k \rho_k u_k}{\partial x} = 0$$
<sup>(2)</sup>

$$\frac{\partial \alpha_k \rho_k u_k}{\partial t} + \frac{\partial \alpha_k \rho_k u_k^2 + \alpha_k P_k}{\partial x} - P_{ik} \frac{\partial \alpha_k}{\partial x} = 0$$
(3)

• For heat transfer, we need an energy equation for each phase.

# **ROE-7 Equations**



### **Different forms of Energy equation**

• Thermodynamics relations

$$m{E}_k = m{e}_k + rac{1}{2}m{u}_k^2$$
 ;  $m{h}_k = m{e}_k + rac{P_k}{
ho_k}$ 

• Total energy

$$\frac{\partial \alpha_k \rho_k E_k}{\partial t} + \frac{\partial \alpha_k \rho_k E_k u_k + \alpha_k P_k u_k}{\partial x} + P_{ik} \frac{\partial \alpha_k}{\partial t} = 0$$
(4)

• Internal energy

$$\frac{\partial \alpha_k \rho_k e_k}{\partial t} + P_{ik} \frac{\partial \alpha_k}{\partial t} + \frac{\partial \alpha_k \rho_k e_k u_k}{\partial x} + P_{ik} u_k \frac{\partial \alpha_k}{\partial x} + \frac{P_k}{\rho_k} \left( \frac{\partial \alpha_k \rho_k u_k}{\partial x} - u_k \frac{\partial \alpha_k \rho_k}{\partial x} \right) = 0$$
(5)

Enthalpy

$$\frac{\partial \alpha_k \rho_k h_k}{\partial t} - \Delta P_k \frac{\partial \alpha_k}{\partial t} - \alpha_k \frac{\partial P_k}{\partial t} + \frac{\partial \alpha_k \rho_k h_k u_k}{\partial x} - u_k \Delta P_k \frac{\partial \alpha_k}{\partial x} - \alpha_k u_k \frac{\partial P_k}{\partial x} = 0$$
(6)  
$$\Rightarrow \Delta P_k = P_k - P_{ik}.$$

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# **ROE-7** Hyperbolicity



#### **Roe-7 model well-posedness**

• To have a well-posed model, the system of equations (SoE) must be hyperbolic. E.g for SoE using total energy, we have

$$\lambda = [u_g - c_g, u_g + c_g, u_g, u_i, u_l - c_l, u_l + c_l, u_l]$$

$$\begin{bmatrix} 1 & 1 & 1 & r_{14} & 0 & 0 & 0 \\ u_g - c_g & u_g + c_g & u_g & r_{14}u_i & 0 & 0 & 0 \\ H_g - u_g c_g & H_g + u_g c_g & H_g - \frac{c_g^2}{\Gamma_g} & r_{34} & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & r_{54} & 1 & 1 & 0 \\ 0 & 0 & 0 & r_{54}u_i & u_l - c_l & u_l + c_l & u_l \\ 0 & 0 & 0 & r_{74} & H_l - u_l c_l & H_l + u_l c_l & H_l - \frac{c_l^2}{\Gamma_l} \end{bmatrix}$$

$$r_{14} = \frac{\rho_g c_g^2 - (\Gamma_g + 1)(P_g - P_{ig})}{c_g^2 - (u_g - u_i)^2}, \quad r_{34} = (H_g - u_g^2 + u_g u_i) r_{14} - P_{ig}$$

$$r_{54} = -\frac{\rho_l c_l^2 - (\Gamma_l + 1)(P_l - P_{il})}{c_l^2 - (u_l - u_l)^2}, \quad r_{74} = -(H_l - u_l^2 + u_l u_i) r_{54} + P_{il}$$



#### Weak Formulation of Roe Scheme

• Since, the governing SoE,  $\frac{\partial \mathbf{U}}{\partial t} + \mathbf{A}(\mathbf{U})\frac{\partial \mathbf{U}}{\partial x} = \mathbf{0}$  is non-conservative, the ROE method cannot be directly used.

$$\mathbf{U} = \begin{bmatrix} \alpha_g \rho_g & \alpha_g \rho_g u_g & \alpha_g \rho_g E_g & \alpha_g & \alpha_l \rho_l & \alpha_l \rho_l u_l & \alpha_l \rho_l E_l \end{bmatrix}^T$$

• Solution: The weak formulation of Roe  $\Rightarrow$  conservative SoE  $\frac{\partial \mathbf{U}}{\partial t} + \frac{\partial \mathbf{F}(\mathbf{U})}{\partial x} = \mathbf{0}$  is approximated by a linear equations system:

$$\frac{\partial \mathbf{U}}{\partial t} + \tilde{\mathbf{A}}(\mathbf{U}_L, \mathbf{U}_R) \frac{\partial \mathbf{U}}{\partial x} = \mathbf{0}$$
(7)

 $\Rightarrow \tilde{\mathbf{A}}$  is the averaged matrix, subscripts L and R denote left and right.

• Averaged matrix must satisfy 3 conditions:

• Hyperbolicity condition. All eigenvalues of **Ã** are real.

- 2 Consistency condition:  $\tilde{\mathbf{A}}(\mathbf{U}_L, \mathbf{U}_R) = \mathbf{A}(\mathbf{U})$
- **3** Jump condition:  $\mathbf{F}(\mathbf{U}_R) \mathbf{F}(\mathbf{U}_L) = \tilde{\mathbf{A}}(\mathbf{U}_L, \mathbf{U}_R)(\mathbf{U}_R \mathbf{U}_L)$



Δu.

### **ROE-7 Averaged Matrix**

• Based on Toumi 92, for a canonical integral path of

$$\mathbf{\Phi}(s;\mathbf{U}_L,\mathbf{U}_R) = \mathbf{U}_L + s(\mathbf{U}_L - \mathbf{U}_R) \tag{8}$$

the averaged matrix is obtained such that

• Once the eigenvalues and right eigenvectors of **Ã** are available, the Riemann problem with the approximated linear equations system can be solved by Godunov method:

$$\mathbf{U}_{i}^{n+1} = \mathbf{U}_{i}^{n} - \frac{\Delta t}{\Delta x} \left( \tilde{\mathbf{A}}_{i+1/2}^{-} (\mathbf{U}_{i+1}^{n} - \mathbf{U}_{i}^{n}) + \tilde{\mathbf{A}}_{i-1/2}^{+} (\mathbf{U}_{i}^{n} - \mathbf{U}_{i-1}^{n}) \right)$$
(10)

## **ROE Linearization**



#### **ROE-7 Averaged Matrix**

• For our SoE, the averaged matrix  $\tilde{\mathbf{A}}$  is

$$\tilde{\mathbf{A}} = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ A_{21} & A_{22} & A_{23} & A_{24} & 0 & 0 & 0 & 0 \\ A_{31} & A_{32} & A_{33} & A_{34} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \bar{u}_i & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & A_{64} & A_{65} & A_{66} & A_{677} \\ 0 & 0 & 0 & A_{74} & A_{75} & A_{76} & A_{77} \end{bmatrix}$$

$$\begin{split} A_{21} &= \frac{\hat{\gamma}_g - 3}{2} \hat{u}_g^2 + (\hat{\gamma}_g - 1)\beta_g & A_{22} = (3 - \hat{\gamma}_g)\hat{u}_g & A_{23} = \hat{\gamma}_g - 1 \\ A_{65} &= \frac{\hat{\gamma}_l - 3}{l_l} \hat{u}_l^2 + (\hat{\gamma}_l - 1)\beta_l & A_{66} = (3 - \hat{\gamma}_l)\hat{u}_l & A_{67} = \hat{\gamma}_l - 1 \\ A_{31} &= (\frac{\hat{\gamma}_g - 1}{2} \hat{u}_g^2 - \hat{H}_g + (\hat{\gamma}_g - 1)\beta_g)\hat{u}_g & A_{32} = \hat{H}_g - (\hat{\gamma}_g - 1)\hat{u}_g^2 & A_{33} = \hat{\gamma}_g \hat{u}_g \\ A_{75} &= (\frac{\hat{\gamma}_l - 1}{2} \hat{u}_l^2 - \hat{H}_l + (\hat{\gamma}_l - 1)\beta_l)\hat{u}_l & A_{76} = \hat{H}_l - (\hat{\gamma}_l - 1)\hat{u}_l^2 & A_{77} = \hat{\gamma}_l \hat{u}_l, \end{split}$$

$$\begin{array}{ll} A_{24} = (\hat{\gamma}_g - 1)\bar{P}_g - \hat{\rho}_g \hat{C}_g^2 + \bar{P}_g - \bar{P}_{ig} & A_{34} = (\hat{\gamma}_g \bar{p}_g - \hat{\rho}_g \hat{C}_g^2)\hat{u}_g - \frac{u_i \bar{P}_{ig}}{u_i \bar{P}_{ig}} \\ A_{64} = \hat{\rho}_l \hat{C}_l^2 - (\hat{\gamma}_l - 1)\bar{P}_l - (\bar{P}_l - \bar{P}_{il}) & A_{74} = (\hat{\rho}_l \hat{C}_l^2 - \hat{\gamma}_l \bar{P}_l)\hat{u}_l + \frac{u_i \bar{P}_{ig}}{u_i \bar{P}_{il}} \end{array}$$

which gives 7 distinct eigenvalues:

$$\lambda = [\hat{u}_g - \hat{C}_g, \ \hat{u}_g + \hat{C}_g, \ \hat{u}_g, \ \bar{u}_l, \ \hat{u}_l - \hat{C}_l, \ \hat{u}_l + \hat{C}_l, \ \hat{u}_l]$$

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#### **Governing Equation**

$$\frac{\partial \alpha_1 \rho_1}{\partial t} + \frac{\partial \alpha_1 \rho_1 u_1}{\partial x} = 0 \tag{11}$$

$$\frac{\partial \alpha_3 \rho_3}{\partial t} + \frac{\partial \alpha_3 \rho_3 u_3}{\partial x} = 0 \tag{14}$$

$$\frac{\partial \alpha_1 \rho_1 u_1}{\partial t} + \frac{\partial \alpha_1 \rho_1 u_1^2 + \alpha_1 P_1}{\partial x} - P_{i12} \frac{\partial \alpha_1}{\partial x} = 0 \quad (12) \quad \frac{\partial \alpha_3 \rho_3 u_3}{\partial t} + \frac{\partial \alpha_3 \rho_3 u_3^2 + \alpha_3 P_3}{\partial x} - P_{i32} \frac{\partial \alpha_3}{\partial x} = 0 \quad (15)$$

$$\frac{\partial \alpha_1 \rho_1 E_1}{\partial t} + \frac{\partial \alpha_1 \rho_1 E_1 u_1 + \alpha_1 P_1 u_1}{\partial x} + P_{i12} \frac{\partial \alpha_1}{\partial t} = 0 \quad (13) \qquad \frac{\partial \alpha_3 \rho_3 E_3}{\partial t} + \frac{\partial \alpha_3 \rho_3 E_3 u_3 + \alpha_3 P_3 u_3}{\partial x} + P_{i32} \frac{\partial \alpha_3}{\partial t} = 0 \quad (16)$$

$$\frac{\partial \alpha_2 \rho_2}{\partial t} + \frac{\partial \alpha_2 \rho_2 u_2}{\partial x} = 0$$
(17)

$$\frac{\partial \alpha_2 \rho_2 u_2}{\partial t} + \frac{\partial \alpha_2 \rho_2 u_2^2 + \alpha_2 P_2}{\partial x} - (P_{i21} + P_{i23}) \frac{\partial \alpha_2}{\partial x} = 0$$
(18)

$$\frac{\partial \alpha_2 \rho_2 E_2}{\partial t} + \frac{\partial \alpha_2 \rho_2 E_2 u_2 + \alpha_2 P_2 u_2}{\partial x} + (P_{i21} + P_{i23}) \frac{\partial \alpha_2}{\partial t} = 0$$
(19)

$$\frac{\partial \alpha_1}{\partial t} + u_{i12} \frac{\partial \alpha_1}{\partial x} = 0$$
<sup>(20)</sup>

$$\frac{\partial \alpha_2}{\partial t} + u_{i23} \frac{\partial \alpha_2}{\partial x} = 0$$
(21)

 $\Rightarrow$  complemented by  $\alpha_1 + \alpha_2 + \alpha_3 = 1$ .

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## **3-Fluid Model**

#### Hyperbolicity



• 11 distinct eigenvalues and eigenvectors  $\Rightarrow$  SoE is hyperbolic.

 $\lambda = [u_1 - c_1, u_1 + c_1, u_1, u_{i12}, u_2 - c_2, u_2 + c_2, u_2, u_{i23}, u_3 - c_3, u_3 + c_3, u_3]$ 0 0  $u_1 - c_1 \quad u_1 + c_1 \quad u_1 \quad u_{i12} r_{14}$ 0 0 0 0 0 0 0 0 0 0 r<sub>58</sub> 0  $\mathbb{R} =$ u<sub>2</sub> u<sub>i23</sub> r<sub>58</sub> 0 0 0 0 0 0 r<sub>77</sub> r<sub>78</sub> 0 1 0 0 0 1 1 1 0 0 0  $u_3 + c_3$ Ui12 194  $u_3 - c_3$ U3 Ô 0 n 0 0 0 r114 r<sub>118</sub> r<sub>119</sub> *r*1110 r11111 

$$\begin{aligned} r_{14} &= \rho_1 c_1^2 - (\Gamma_1 + 1)(P_1 - P_{i12})/(c_1^2 - (u_1 - u_{i12})^2), \quad r_{34} = (H_1 - u_1^2 - u_1 u_{i12}) r_{14} - P_{i12} \\ r_{94} &= -(\rho_3 c_3^2 - (\Gamma_3 + 1)(P_3 - P_{i32}))/(c_3^2 - (u_3 - u_{i12})^2), \quad r_{114} = -(H_3 - u_3^2 - u_3 u_{i12}) r_{94} + P_{i32} \\ r_{58} &= \rho_2 c_2^2 - (\Gamma_2 + 1)(P_3 - P_{i21} - P_{i23})/(c_2^2 - (u_2 - u_{i23})^2), \quad r_{78} = (H_2 - u_2^2 - u_2 u_{i23}) r_{14} - P_{i21} - P_{i23} \\ r_{98} &= -(\rho_3 c_3^2 - (\Gamma_3 + 1)(P_3 - P_{i32}))/(c_3^2 - (u_3 - u_{i23})^2), \quad r_{118} = -(H_3 - u_3^2 - u_3 u_{i23}) r_{98} + P_{i32} \end{aligned}$$